

Study of Effective Dielectric Permittivity and Capacitance for Finite Dielectric Thickness Coplanar Waveguide

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Abstract

At higher frequencies microwave and millimeter wave transmission lines play an important role. Among all transmission lines CPW is rapidly becoming salient substitute due to its uniplanar geometry. In this paper simulation and Analysis (quasi static analysis using conformal mapping) of FCPW (Finite dielectric thickness Coplanar Waveguide) on Alumina and Rogers substrate with varying height of substrate are analyzed. The effect of Capacitance and effective permittivity on aspect ratio is also analyzed. Simulations are carried out on SONNET software; it is based upon Method of Moments principle and gives excellent simulations which are consistent with actual fabrications. This paper will help to optimize the design and fabrication of the FCPW for various dedicated applications.

Keywords

Coplanar Waveguide, Transmission Line, Quasi Static Analysis, Conformal Mapping, SONNET.

I. Introduction

In amplified use of hybrid, monolithic microwave and millimeter wave circuits the choice of transmission line is coplanar waveguide (CPW). It is the most striking alternative to conventional used microstrip line and stripline due to its uniplanar geometry. It consist of a centre strip with two ground planes located in the same plane [1-2] i.e., on the same surface of dielectric slab as shown in Figure.1. The ground plane being on the same surface lends itself to easy mounting of circuit elements and active devices; Drilling of holes or slots through the substrate is not needed [3-6].

CPW structures are commonly used in high-speed circuits and interconnect. It offers several advantages over microstrip which are summarized in Table 1. The use of CPW in the design of circuit components and transmission lines is not yet widespread. One reason for this is due to the lack of analytical data pertaining to the characteristics of CPW [7-8].

The electromagnetic wave carried by a coplanar waveguide exists to a certain extent in the dielectric substrate, and partly in the air above it, electric and magnetic field distribution is shown in fig. 2.

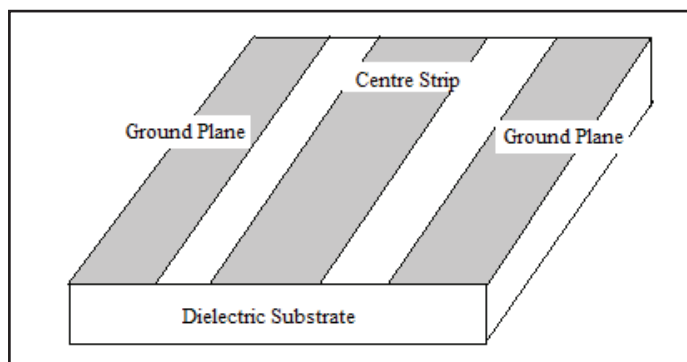


Fig. 1: Conventional Coplanar Waveguide Structure

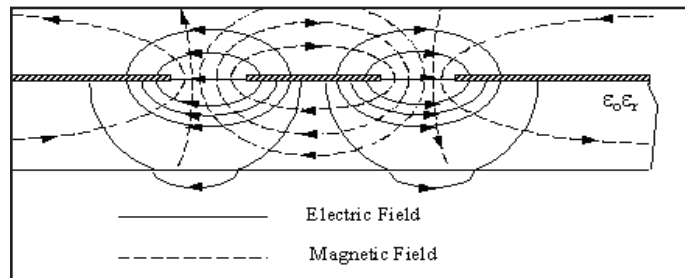


Fig. 2: Electric and Magnetic Field Distribution in CPW

Table 1: Comparison Between Microstrip line and CPW

| Properties | Microstrip | CPW |
|--------------------|------------|-------|
| Dispersion | High | Low |
| Losses | Low | High |
| Coupling | High | Low |
| Design flexibility | Low | High |
| Circuit size | Large | Small |
| Via holes | Yes | No |

In general, the dielectric constant of the substrate will be different than that of the air, so that the wave is travelling in an inhomogeneous medium [9-12]. As a consequence CPW will not support an exact TEM mode; at non-zero frequencies. At low frequencies, both loss and dispersion are limited and this mode is frequently called “quasi-TEM” mode because its propagation characteristics are similar to the TEM mode [13,18].

II. Materials and Methods

A. Alumina Substrate

Alumina is the ceramic form of sapphire. It has balanced properties of insulation, thermal conductivity and breaking strength. It is usually available in white color having dielectric constant varying from 9.5 to 10 with loss tangent $\tan\delta = 0.0002$. Its unique property is surface roughness and excellent adhesion with a thin film and thick film metallization due to fine particles. Various advantages of Alumina are: Physical and chemical properties are stable even at very high temperatures, High Mechanical strength, Good in insulation properties, Less porous with good smoothness. Gold metallization is frequently used with alumina. Usually a very thin adhesion layer is used between alumina and gold.

B. Rogers Substrate

This is Temperature Stable Microwave Laminates which are available in a wide range of dielectric constants. TMM (Thermoset Microwave Materials) are ceramic, hydrocarbon, polymer composites designed for high plated-thru-hole transmission line applications. The electrical and mechanical properties of TMM laminates unite many of the benefits of both ceramic as well as traditional PTFE microwave circuit laminates without requiring

the specialized production techniques [15]. We have used TMM6 with dielectric constant equal to 6.0 ± 0.080 .

III. Quasi Static Analysis

A CPW can be quasi-statically analyzed by the use of conformal mapping. The closed form design equation obtained by conformal mapping method which is simplest and most often used method consists of complete elliptic integral which are difficult to calculate [1-2]. Thus approximate formulas are proposed for the calculation of elliptical integral by conformal mapping. For analysis of CPW with finite dielectric substrate we have to assume capacitance due to lower half plane is sum of free space and dielectric layer capacitance with permittivity $(\epsilon_r - 1)$. Conformal Transformation is used to transform CPW into parallel plate structure [7-8]. The capacitance due to upper half plane is given by:

$$C_1 = 2\epsilon_0 \frac{K(k_1)}{K'(k_1)}$$

The transformation is:

$$t_1 = \sinh\left(\frac{\pi a}{2h}\right)$$

and

$$t_2 = \sinh\left(\frac{\pi b}{2h}\right)$$

Therefore Capacitance is given by:

$$C_2 = 2\epsilon_0(\epsilon_r - 1) \frac{K(k_2)}{K'(k_2)}$$

Where k_1, k_2 are elliptical integrals

The total capacitance is given by

$$C = 2C_1 + C_2$$

We can also obtain ϵ_{re} by following equation:

$$\epsilon_{re} = 1 + q(\epsilon_r - 1)$$

Where filling factor 'q' is given by:

$$q = \frac{1}{2} \frac{K(k_2)}{K'(k_2)} \frac{K'(k_1)}{K(k_1)}$$

IV. Structure and Design

For practical applications it is impossible to take dielectric substrate and ground planes to be infinite so CPW with finite dielectric substrate and finite width ground planes are required for many practical applications [14]. The CPW analyzed in this paper is Finite substrate thickness CPW as shown in fig. 3. In this structure centre strip conductor with two ground planes on either side mounted on dielectric substrate with height of dielectric layer taken as 'h' [1] [16].

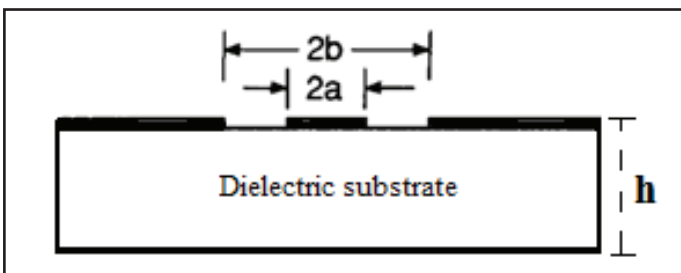


Fig. 3: CPW with Finite Dielectric Substrate

In this study Height of substrate and gap between ground plane and centre strip is varied which is listed in Table 2 & 3 for Alumina and Rogers Substrate respectively. The effects of height of substrate and gap between strip and ground plane have also been analyzed.

Table 2: Dimensions of CPW with Alumina as Dielectric Substrate

| S. No. | Height of Substrate(h) in mm | Gap(g) in mm | Width(w) in mm |
|--------|------------------------------|--------------|----------------|
| 1. | h=0.4 | 0.15 | 0.28 |
| | | 0.3 | 1.02 |
| 2. | h=0.28 | 0.15 | 0.32 |
| | | 0.3 | 1.47 |
| 3. | h=0.19 | 0.15 | 0.42 |
| | | 0.3 | 2.2 |

Table 3: Dimensions of CPW with Rogers TMM1 as Dielectric Substrate

| S. No. | Height of Substrate(h) in mm | Gap(g) in mm | Width(w) in mm |
|--------|------------------------------|--------------|----------------|
| 1. | h=0.381 | 0.15 | 0.76 |
| | | 0.30 | 2.99 |
| 2. | h=0.508 | 0.15 | 0.67 |
| | | 0.30 | 2.4 |
| 3. | h=0.762 | 0.15 | 0.62 |
| | | 0.30 | 1.84 |

V. Result and Discussion

Fig. 4 (a) & (b) shows 2D & 3D model for FCPW respectively obtained through SONNET software simulation [17]. Simulation is done on Alumina and Rogers substrate with $\epsilon_r = 9.8$, loss tangent $\tan\delta = 0.0002$ and $\epsilon_r = 6.0$, loss tangent $\tan\delta = 0.0023$ respectively. The simulated parametric study results and conformal mapping analysis for FCPW are obtained. Graph shown below represents the effect of aspect ratio and gap between strip and ground plane on capacitance, Effective dielectric permittivity, transmission coefficient and reflection coefficient for varying height of substrates.

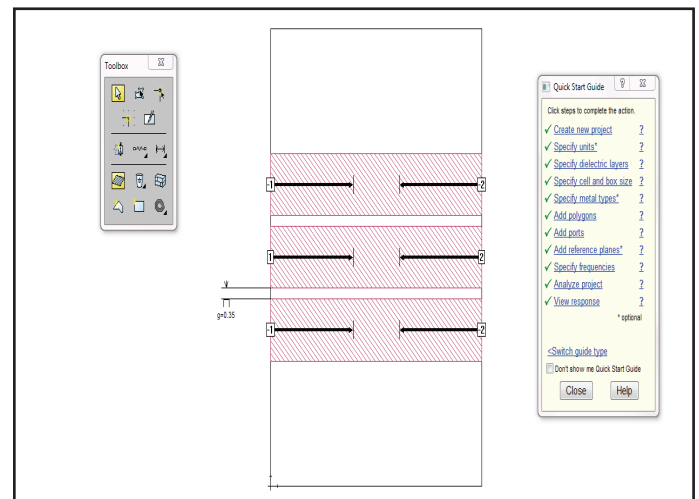


Fig. 4: (a) 2-D model of FCPW

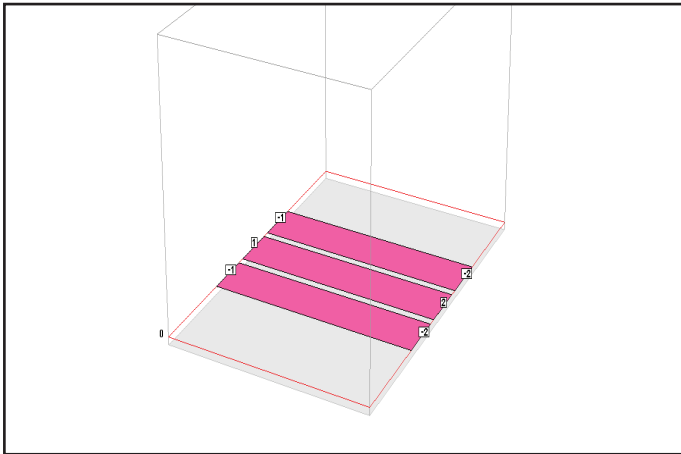


Fig. 4: (b) 3-D model of FCPW

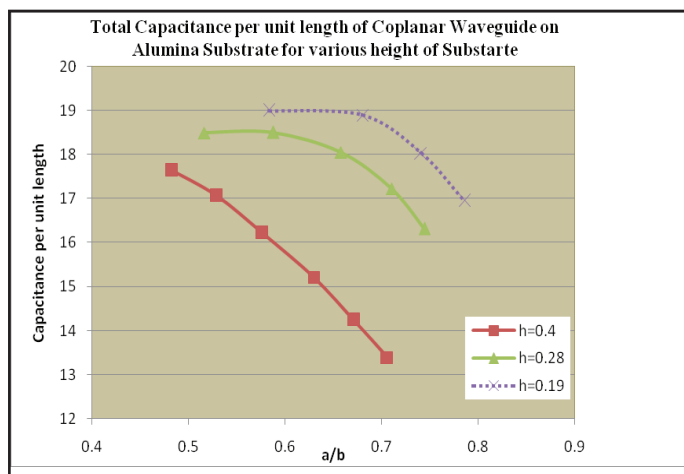


Fig. 5: (a) Variation of Capacitance with aspect ratio for varying height of Alumina Substrate

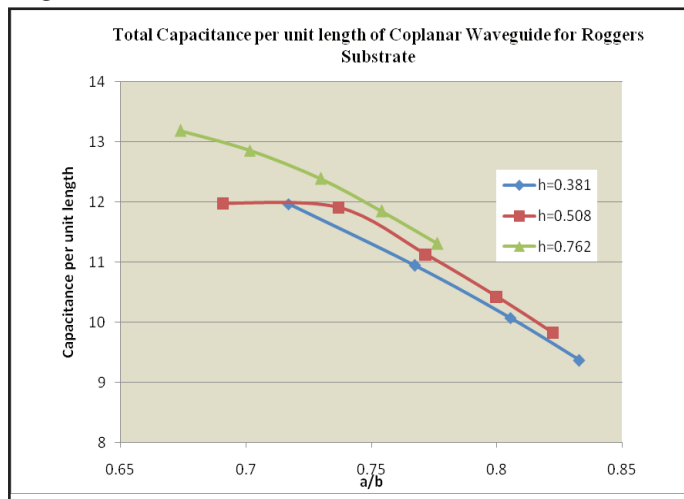


Fig. 5 (b): Variation of Capacitance With Aspect Ratio for Varying Height of Rogers Substrate

Fig. 5(a) and Fig. 5(b) shows the capacitance versus a/b for Alumina and Rogers Substrate respectively. From figure it is clear that the capacitance of FCPW is sensitive to change in aspect ratio. From quasi static analysis it is seen that Capacitance decreases with increasing a/b . And the slope of curve almost remains same for all heights. As height of the substrate increases, its capacitance decreases.

Fig. 6 (a) and 6 (b) shows the effective dielectric permittivity versus a/b for Alumina and Rogers substrate respectively. From

the graph it is clear that the effective dielectric permittivity (ϵ_{eff}) is also sensitive to change in aspect ratio. From quasi static analysis it is seen that ϵ_{eff} decreases with increasing a/b . And the slope of curve almost remains same for all heights. As height of substrate increases effective dielectric permittivity decreases.

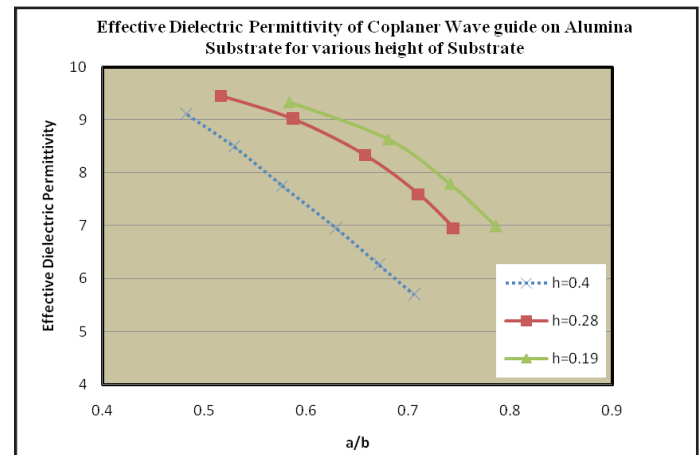


Fig. 6: (a) Variation of Effective Dielectric Permittivity With Aspect Ratio for Varying Height of Alumina Substrate

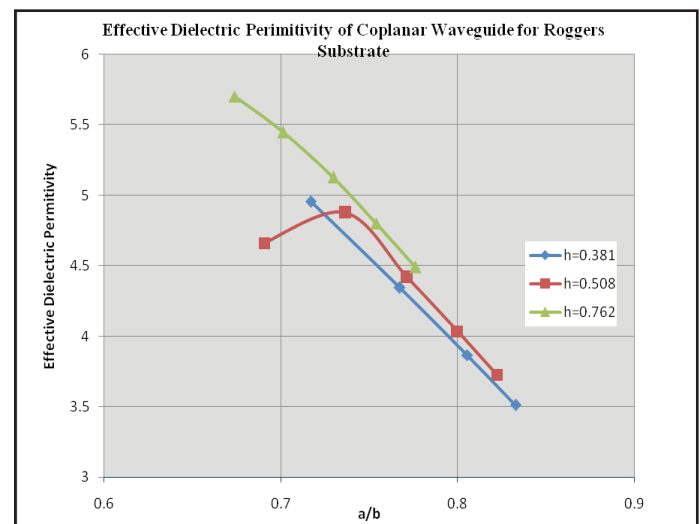


Fig. 6: (b) Variation of Effective Dielectric Permittivity with aspect ratio for varying height of Rogers Substrate

Fig. 7 (a) and (b) shows the Capacitance versus Gap for Alumina and Rogers Substrate respectively and fig. 8 (a) and (b) shows the effective dielectric permittivity versus Gap for Alumina and Rogers Substrate respectively.

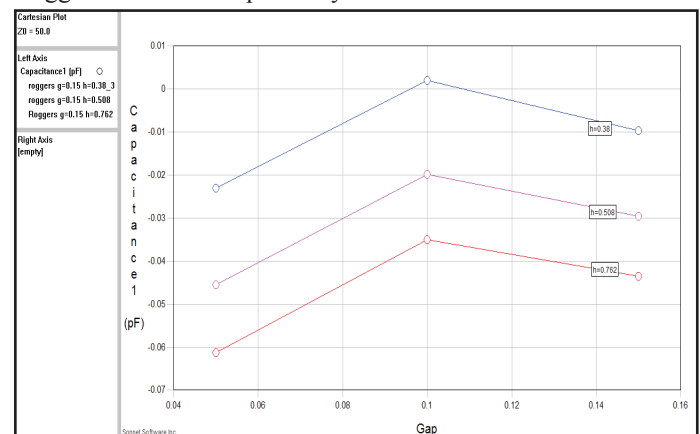


Fig. 7: (a) Variation of Capacitance with gap (mm) for varying height of Alumina Substrate

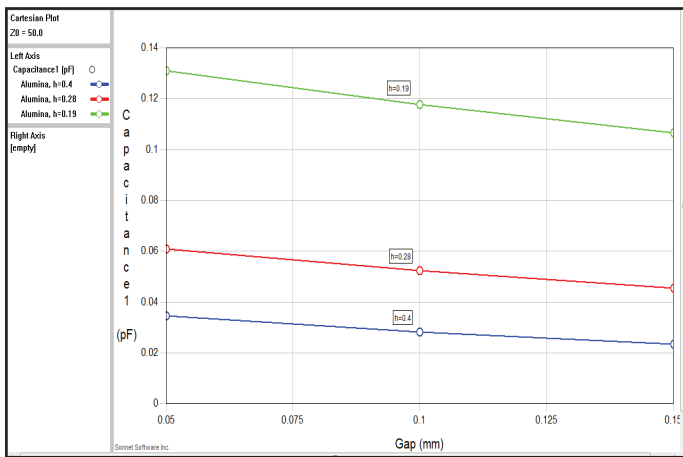


Fig. 7: (b) Variation of Capacitance with gap (mm) for varying height of Rogers Substrate

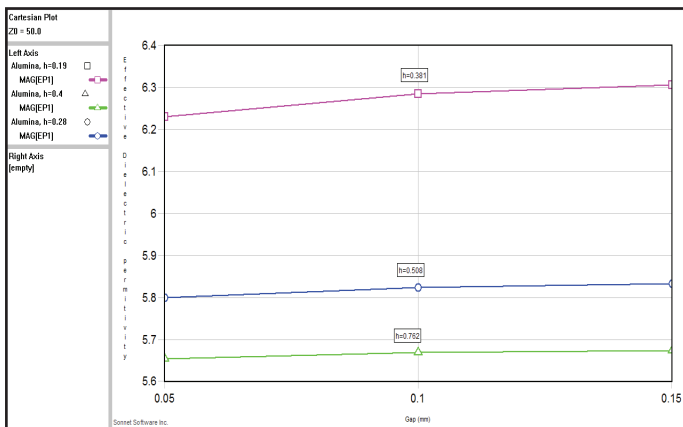


Fig. 8: (a) Variation of Effective Dielectric Permittivity with gap (mm) for varying height of Alumina Substrate

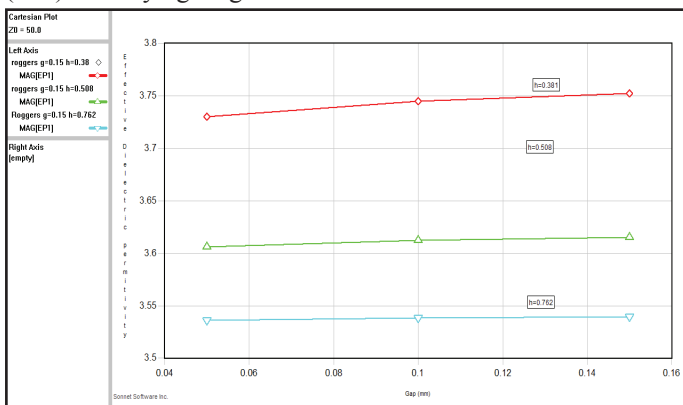


Fig. 8: (b) Variation of Effective Dielectric Permittivity with gap (mm) for Varying Height of Rogers Substrate

From simulations it is seen that capacitance and effective dielectric permittivity changes with varying gap between strip and ground plane. Capacitance sequentially decreases for Alumina then for Rogers substrate while effective dielectric permittivity remains almost same with increasing gap between strip and ground plane for both substrates at all heights of substrate.

Fig. 9. (a) and (b) shows the Transmission coefficient versus Gap for Alumina and Rogers Substrate respectively and fig. 10 (a) and (b) shows the Reflection Coefficient versus Gap for Alumina and Rogers Substrate respectively. Reflection and transmission coefficients are also plotted through simulations. It is found that for Rogers, the transmission coefficient decreases with gap while

for alumina it increases and reflection coefficient varies almost same for both the substrates.

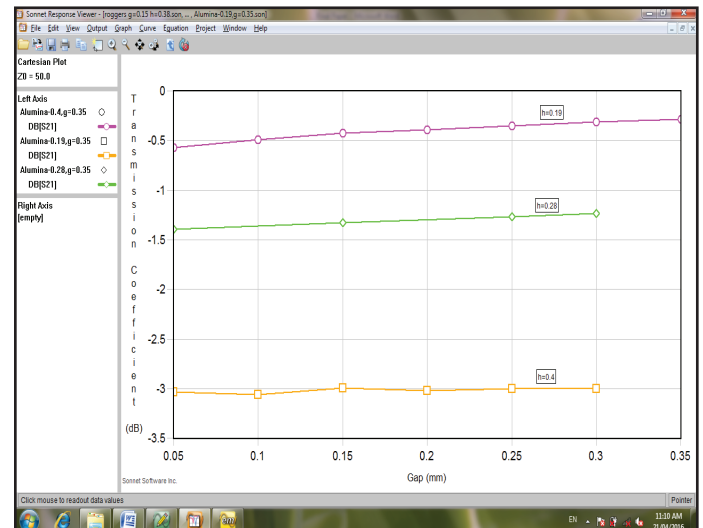


Fig. 9: (a) Variation of Transmission Coefficient with gap (mm) for varying height of Alumina Substrate

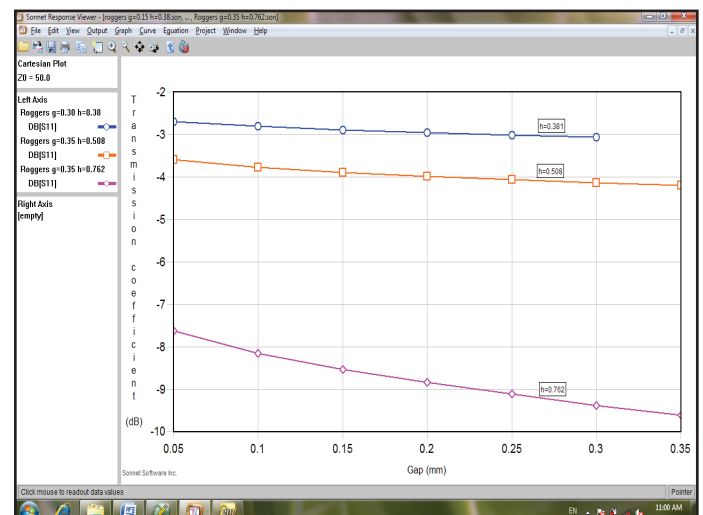


Fig. 9: (b) Variation of Transmission Coefficient with gap (mm) for varying height of Rogers Substrate

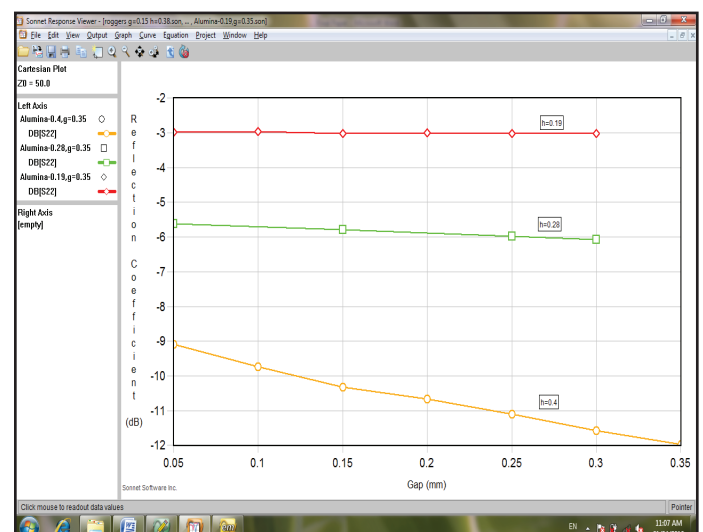


Fig. 10: (a) Variation of Reflection Coefficient with gap (mm) for varying height of Alumina Substrate

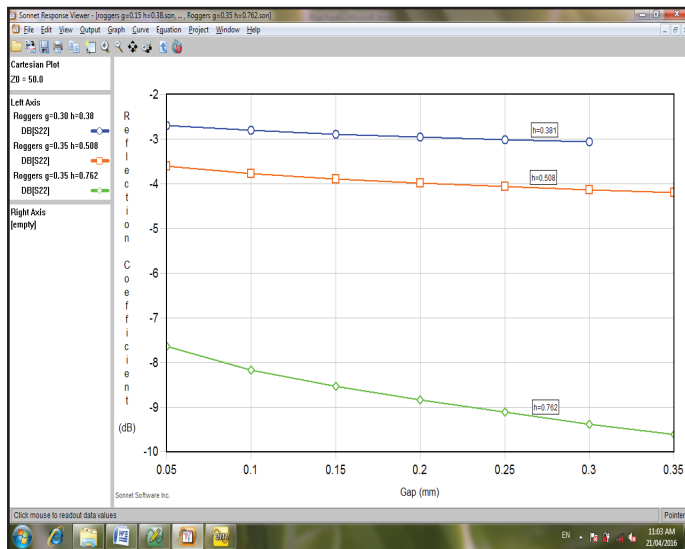


Fig. 10: (b) Variation of Reflection Coefficient with gap (mm) for varying height of Rogers Substrate

VI. Conclusion

This study reports the quasi static analysis and parametric study of FCPW. Hence it is concluded that in the process of FCPW's fabrication special attention needs to be taken about height of substrate and gap. FCPW is modeled through simulation which shows that alumina favors sequential decrease of capacitance, increase of transmission and decrease of reflection coefficient for varying heights.

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